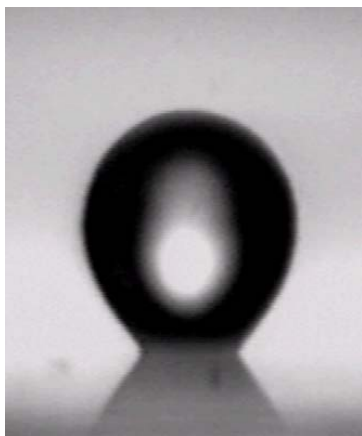


# Detachment of **Oil Drops** from **Solid Surfaces** in **Surfactant Solutions**: Molecular Mechanisms at a **Moving Contact Line**

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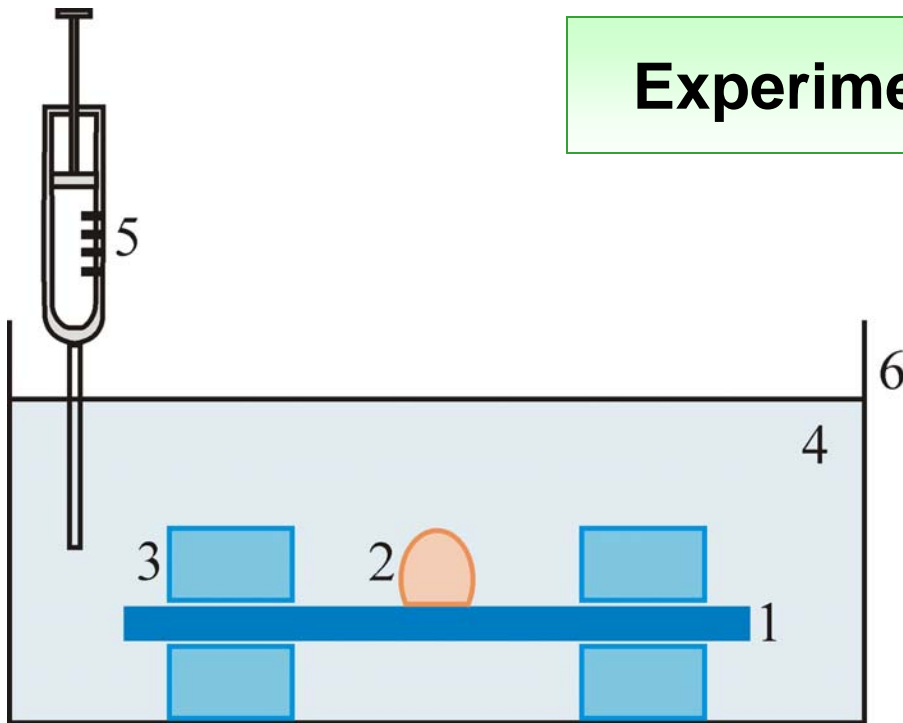


Drop detachment:  
**Moving contact line**;  
Importance for **Detergency**;  
**Membrane emulsification**;  
Other processes with **moving**  
three-phase contact line

**Aim:** (i) Examine the effect of **temperature**, **surfactant** and **salt** concentrations, on the dynamics of drop detachment.

(ii) Develop of a quantitative **theoretical model**; **fit** the experimental data; determine the values of the involved physicochemical parameters.

## Experiment



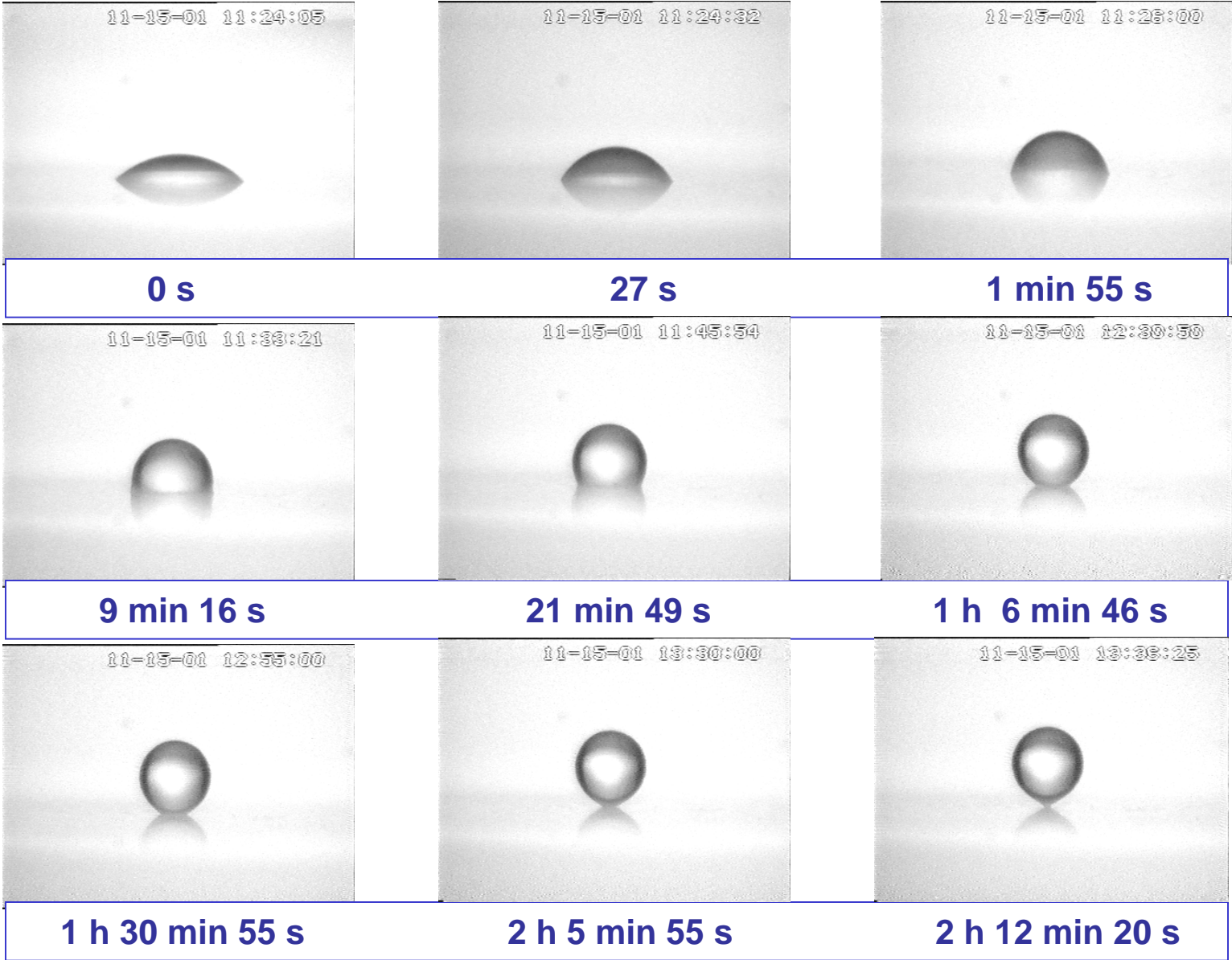
Scheme of the experimental cell:

- 1 – glass plate;
- 2 – oil droplet  $\approx 1 \mu\text{l}$ ;
- 3 – glass holders;
- 4 – surfactant solution;
- 5 – syringe; 6 – cuvette.

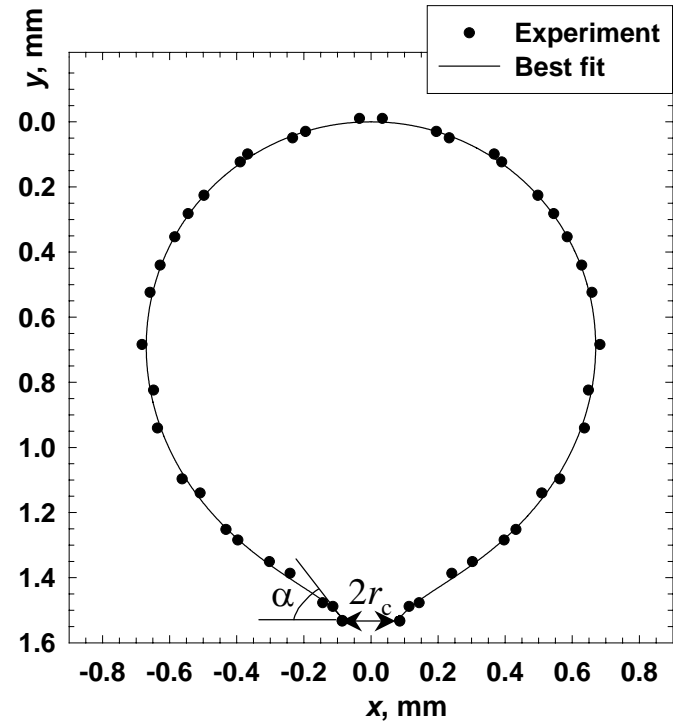
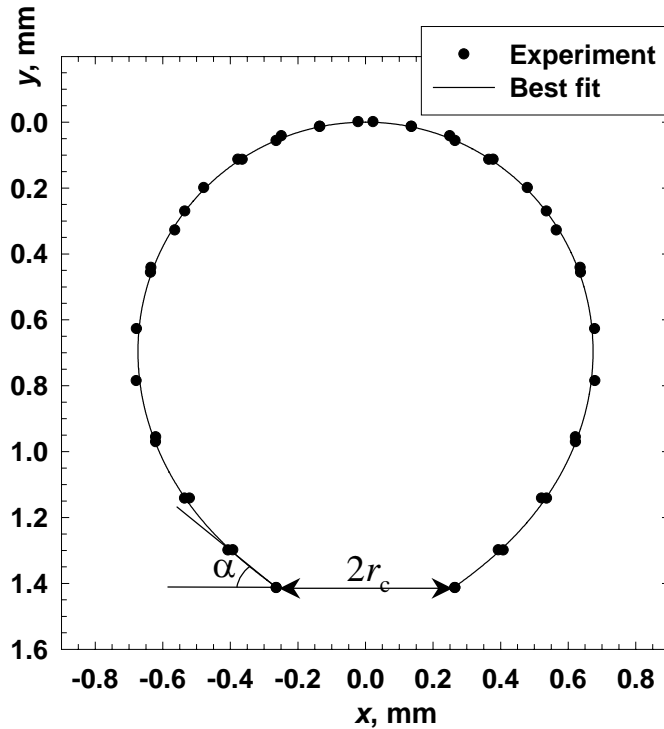
### Procedure:

- (1) Oil drop is placed on the dry glass substrate;
- (2) Solution of surfactant + NaCl is poured in the cuvette;
- (3) The process of oil drop detachment is recorded by horizontal microscope and video-camera.

# Dynamics of Spontaneous Drop Detachment



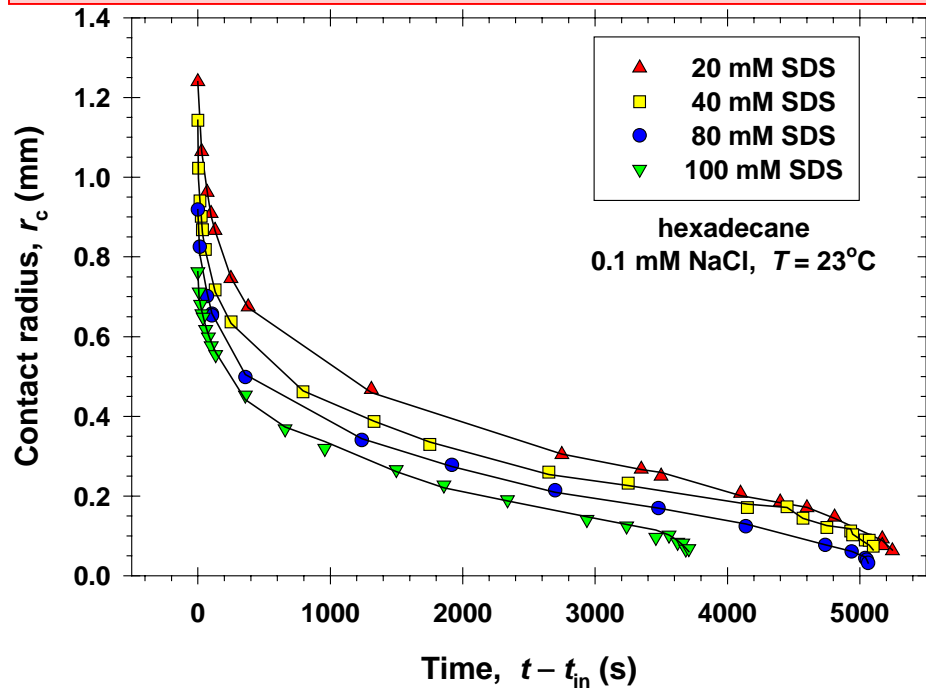
## Drop Profile: Digitization and Fit by Laplace Equation



Results from the fit:

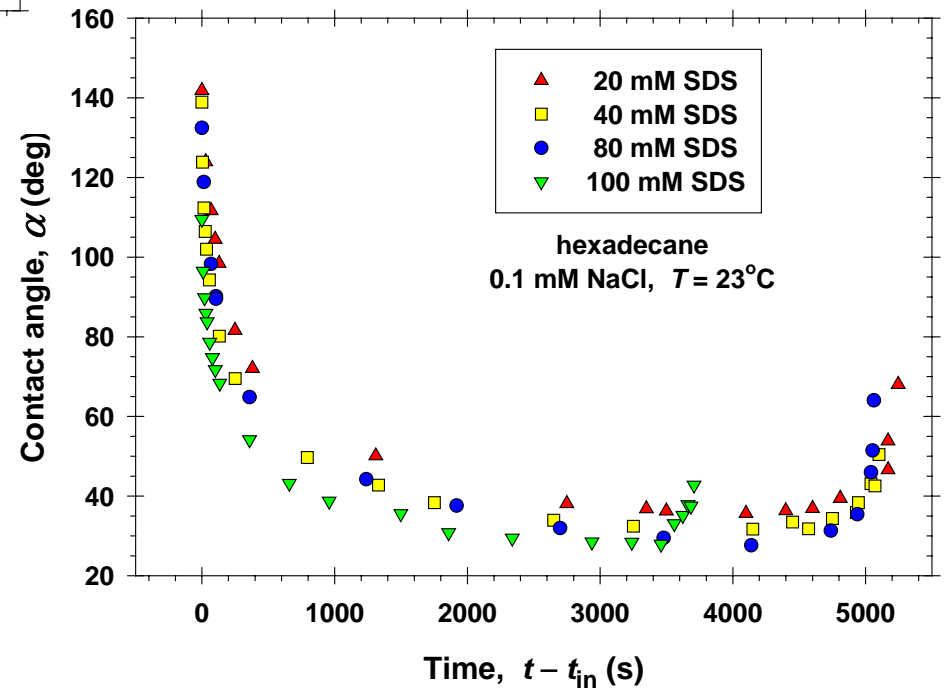
Determination of the **contact radius,  $r_c$** , and **contact angle,  $\alpha$** ,  
as functions of **time,  $t$** .

## Effect of SDS concentration on detachment of **hexadecane** drops from **glass**:

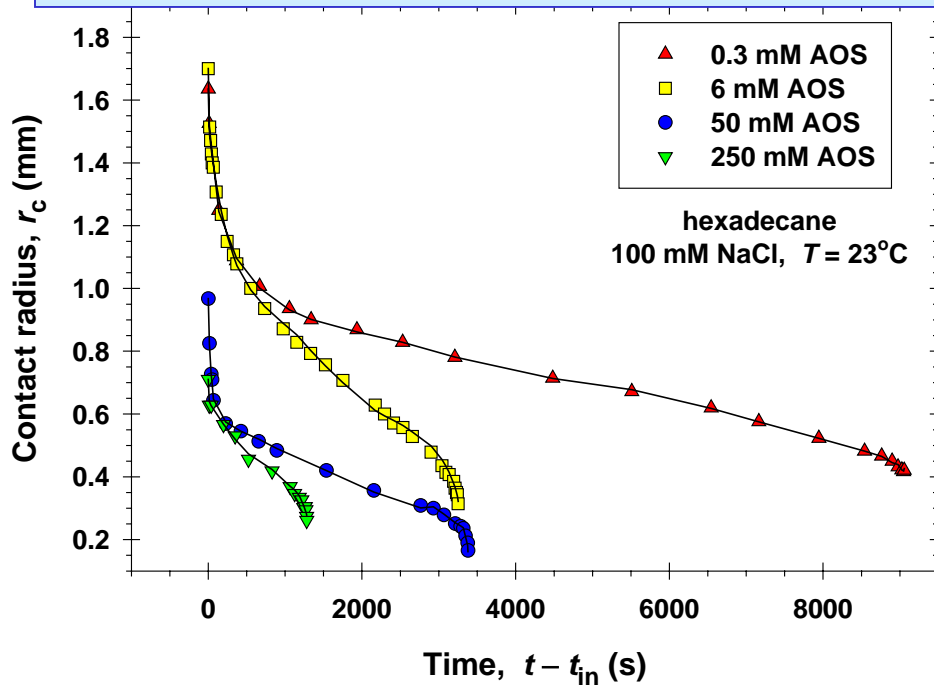


Data for the **contact radius**,  $r_c$ , and for the **contact angle**,  $\alpha$ , plotted vs. time; the initial moment,  $t_{in}$ , corresponds to the first experimental point. The **NaCl concentration is 0.1 mM** and the **temperature is  $23^\circ\text{C}$** .

The increase of the **SDS (sodium dodecyl sulfate)** concentration accelerates the oil-drop detachment.

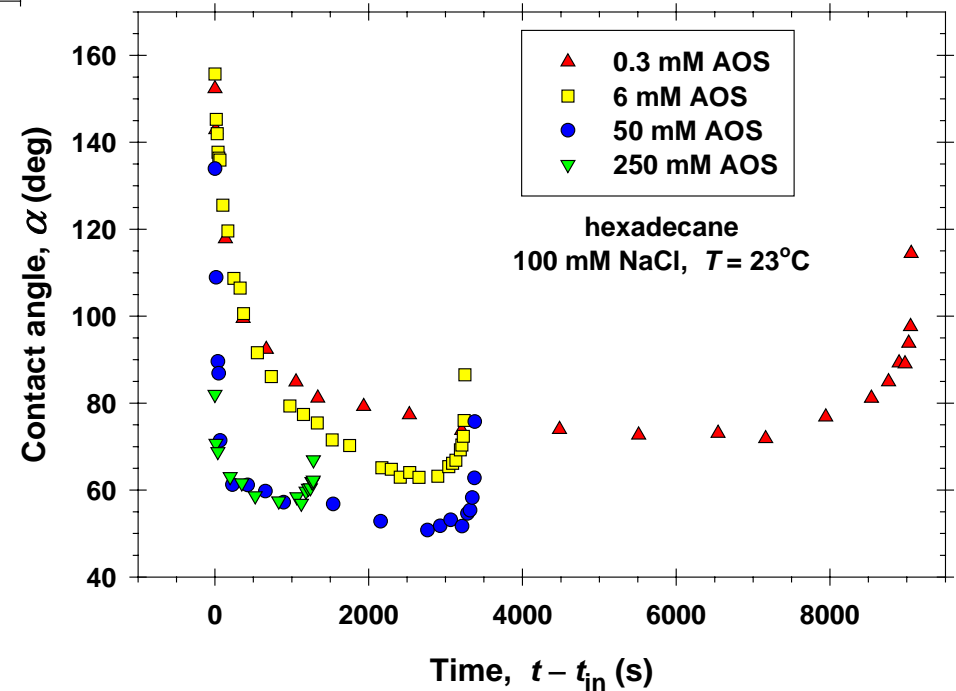


## Effect of **AOS** concentration on detachment of **hexadecane** drops from **glass**:

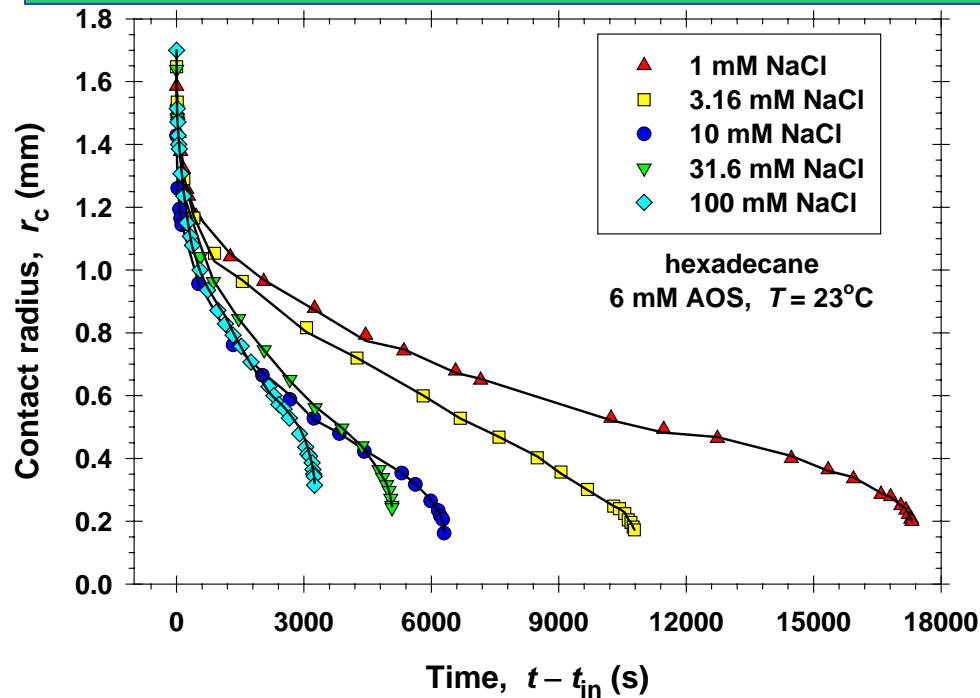


Data for the **contact radius**,  $r_c$ , and for the **contact angle**,  $\alpha$ , plotted vs. time; the initial moment,  $t_{in}$ , corresponds to the first experimental point. The **NaCl concentration is 100 mM** and the **temperature is  $23^{\circ}\text{C}$** .

The increase of the **AOS** (sodium  $\text{C}_{16}$  alpha-olefin-sulfonate) concentration accelerates the oil-drop detachment.

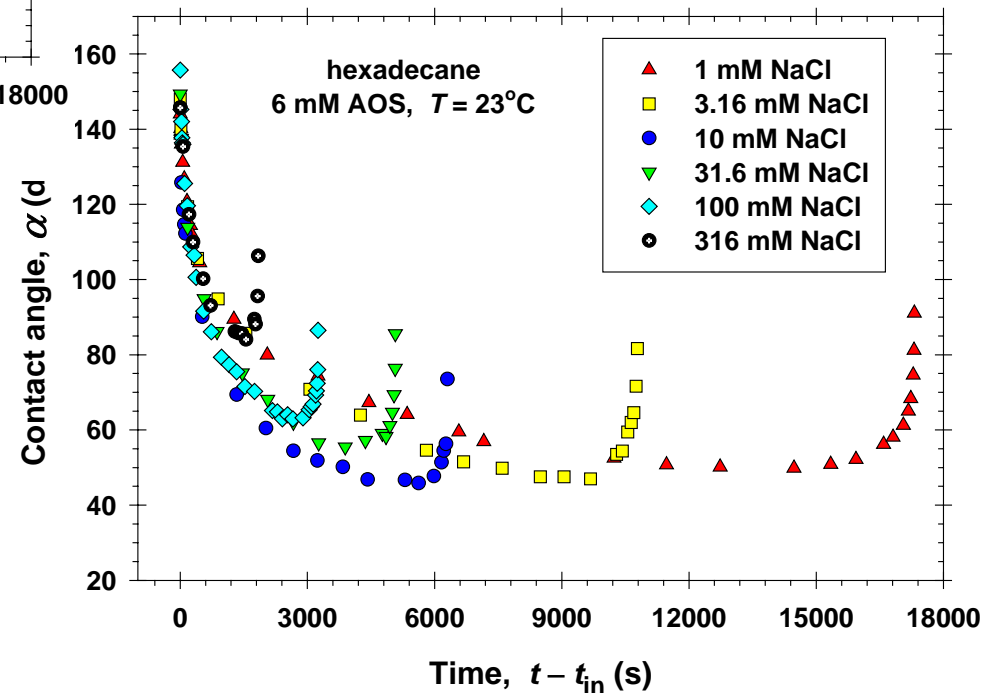


## Effect of **NaCl** concentration on detachment of **hexadecane** drops from **glass**:

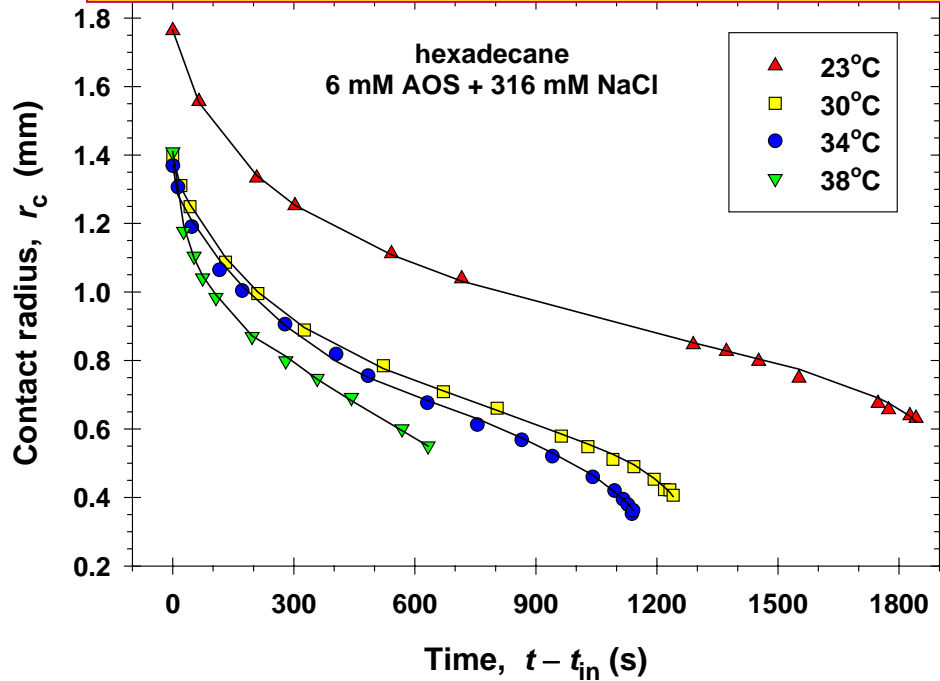


Data for the **contact radius**,  $r_c$ , and for the **contact angle**,  $\alpha$ , plotted vs. time; the initial moment,  $t_{in}$ , corresponds to the first experimental point. The **AOS concentration is 6 mM** and the **temperature is  $23^\circ\text{C}$** .

The increase of the **NaCl** concentration accelerates the oil-drop detachment.

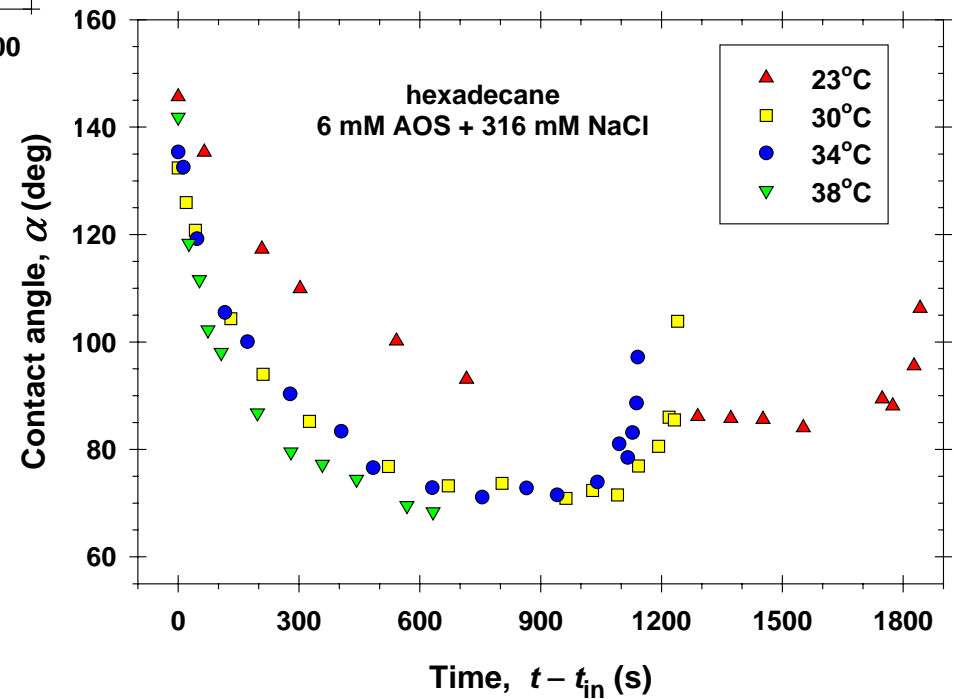


## Effect of temperature on detachment of **hexadecane** drops from **glass**:



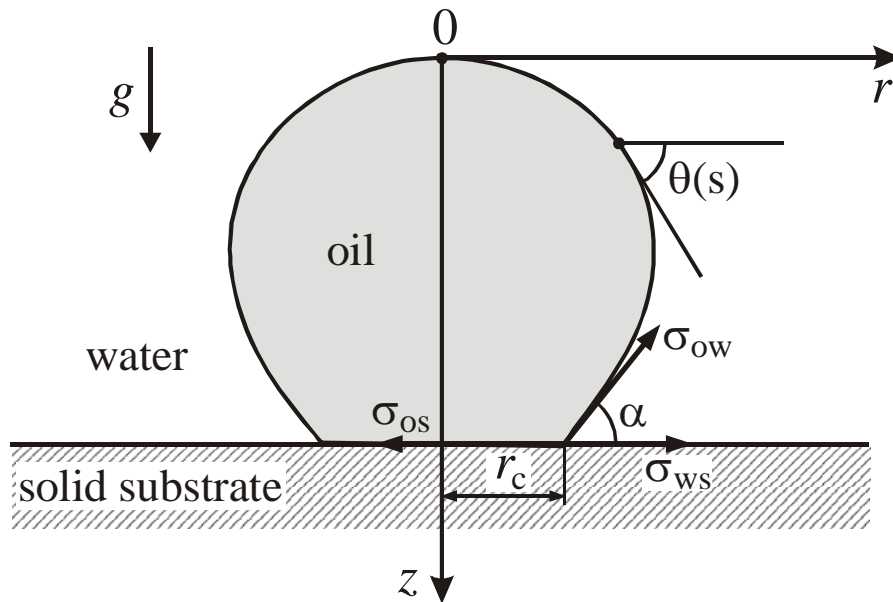
Data for the **contact radius**,  $r_c$ , and for the **contact angle**,  $\alpha$ , plotted vs. time; the initial moment,  $t_{in}$ , corresponds to the first experimental point. The **AOS concentration is 6 mM** and the **NaCl concentration is 316 mM**.

The increase of the **temperature** accelerates the oil-drop detachment.





## Theoretical Basis



At equilibrium:  
the **Young equation** holds

$$\sigma_{os} = \sigma_{ws} + \sigma_{wo} \cos \alpha_{eq}$$

During relaxation:  
the **Young equation** contains an additional **friction term**, which compensates the imbalance of the three interfacial tensions:

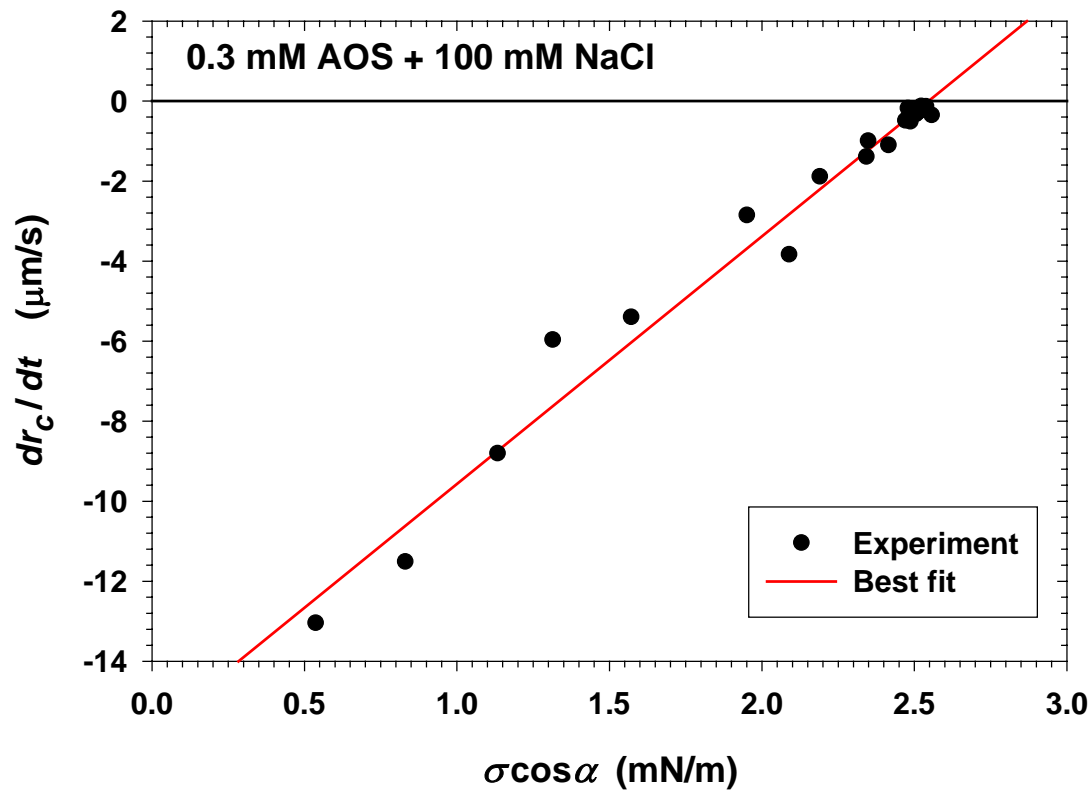
$$\beta \frac{d r_c}{d t} = \sigma_{ow} \cos \alpha + \sigma_{ws} - \sigma_{os}$$

$\beta$  is the line friction coefficient

## Determination of the Line Friction Coefficient

$$\frac{d r_c}{d t} = \frac{1}{\beta} (\sigma_{ow} \cos \alpha + \sigma_{ws} - \sigma_{os})$$

Set of preliminary data:  
glass plates cleaned by **sulfo-  
chromic acid**



From the slope of the best fit  
we determine the line friction  
coefficient:

$$\beta = 1.6 \text{ Pa}\cdot\text{s}$$

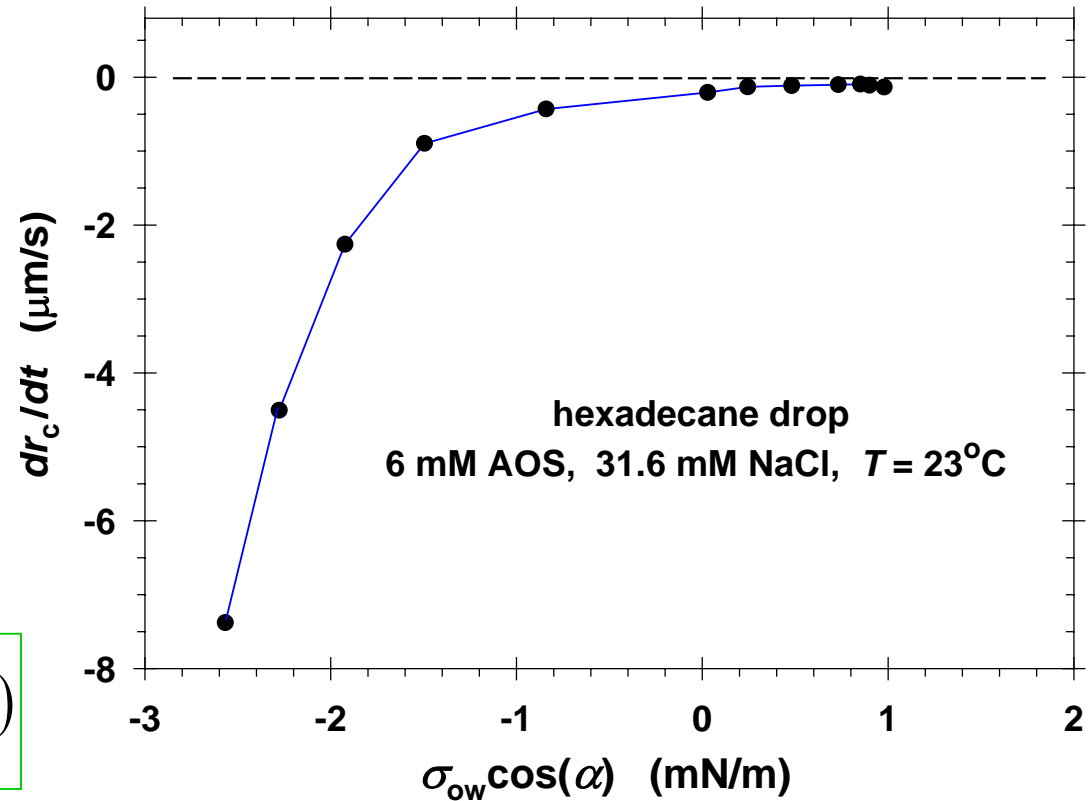
Basic question:

How does  $\beta$  depend on  
surfactant and salt  
concentrations and on the  
temperature?

## New Set of Data

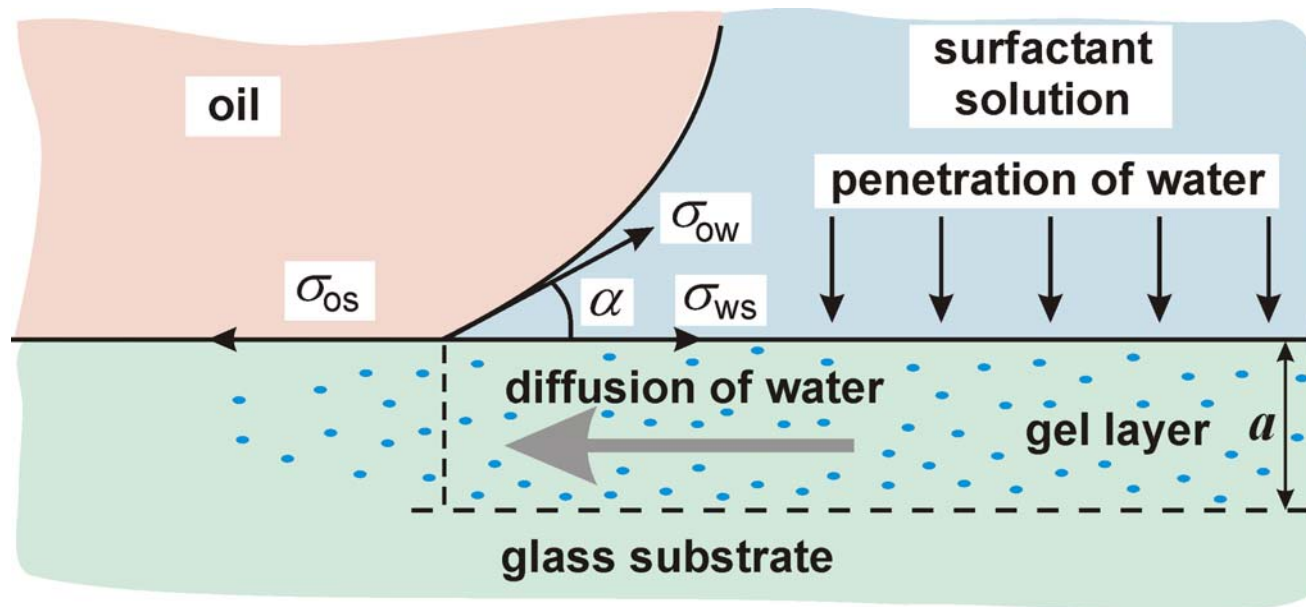
The **glass plates** are used as provided by the producer; **no** cleaning by **sulfo-chromic acid**

$$\frac{d r_c}{d t} = \frac{1}{\beta} (\sigma_{ow} \cos \alpha + \sigma_{ws} - \sigma_{os})$$



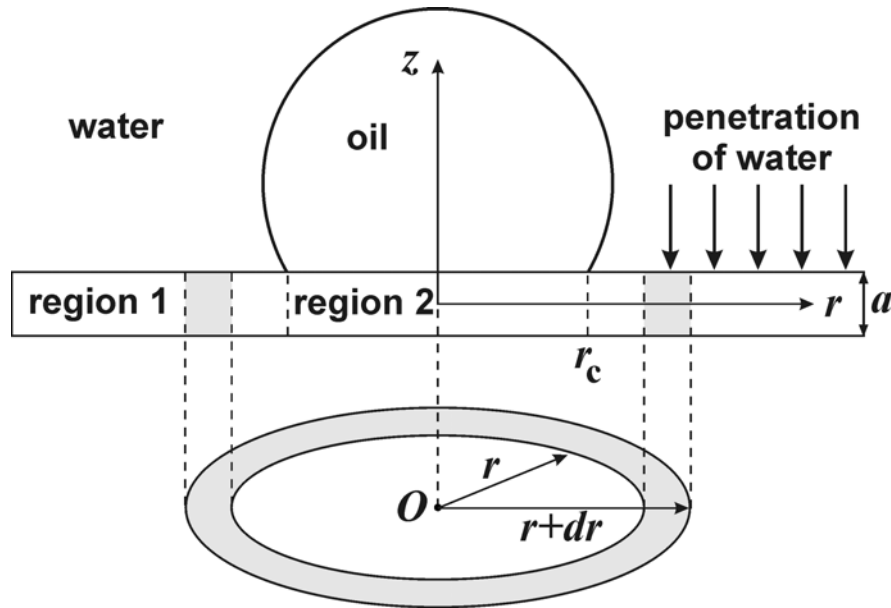
**The** difference  $\sigma_{os} - \sigma_{ws}$  is not constant, but varies with time: Consequence of the formation of a **gel layer** on the **glass surface** in contact with water.

**Data Interpretation: Diffusion of water into the surface layer of glass and development of a gel layer**



**Theoretical model** is developed, which accounts for the penetration and **diffusion of water in the surface of glass**, and for the **dependence of  $\sigma_{os}$  and  $\sigma_{ws}$**  on the concentration of water in the gel layer at the contact line.

## Theoretical Model



Diffusion equation for **region 2**

$$\frac{\partial c_2}{\partial t} = \frac{D}{r} \frac{\partial}{\partial r} \left( r \frac{\partial c_2}{\partial r} \right) \quad (0 < r < r_c)$$

Concentrations and fluxes equal at the boundary **region 1 / region 2**

Limiting case of **fast** diffusion:

$$c_b(t) = \frac{c_{eq}}{2} \left[ 1 - \exp\left(-\frac{t}{t_p}\right) \right]$$

$$\frac{\partial c_1}{\partial t} = \frac{D}{r} \frac{\partial}{\partial r} \left( r \frac{\partial c_1}{\partial r} \right) + \frac{1}{t_p} (c_{eq} - c_1) \quad (r > r_c)$$

Diffusion equation for **region 1** (the last term accounts for the influx from the water phase);

- D** – diffusivity of water in the gel layer;
- c** – concentration of water in the gel layer;
- t<sub>p</sub>** – characteristic penetration time.

- c<sub>b</sub>** – concentration of water at the boundary between regions 1 and 2 (at  $r = r_c$ );
- c<sub>eq</sub>** – equilibrium value of **c**.

## Comparison of Theory and Experiment

We assume a simple **Henry law** for the interfacial tensions:

$$\sigma_{ws} = \sigma_{ws}(0) - \lambda_{ws} c_b$$

$$\sigma_{os} = \sigma_{os}(0) + \lambda_{os} c_b$$

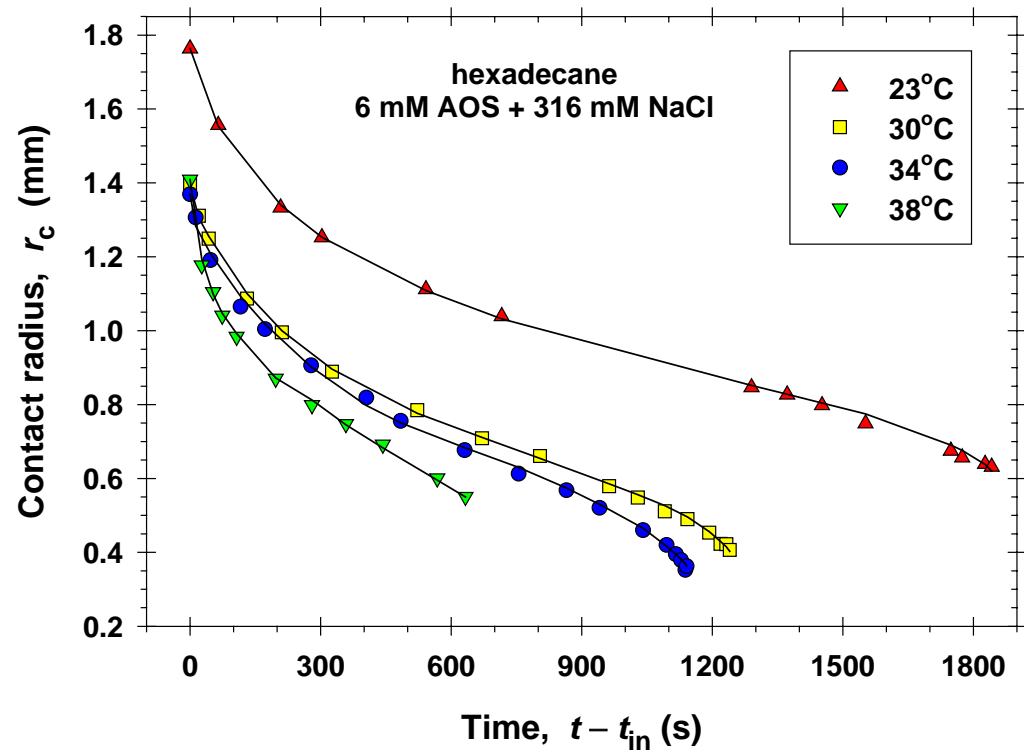
Integrated **equation of contact-line motion**:

$$r_c(t) = r_c(0) + \frac{\sigma_{ow}}{\beta} \int_0^t \cos \alpha(\hat{t}) d\hat{t} - \frac{\Delta\sigma}{\beta} t + \frac{\gamma t_p}{\beta} [1 - \exp(-\frac{t}{t_p})]$$

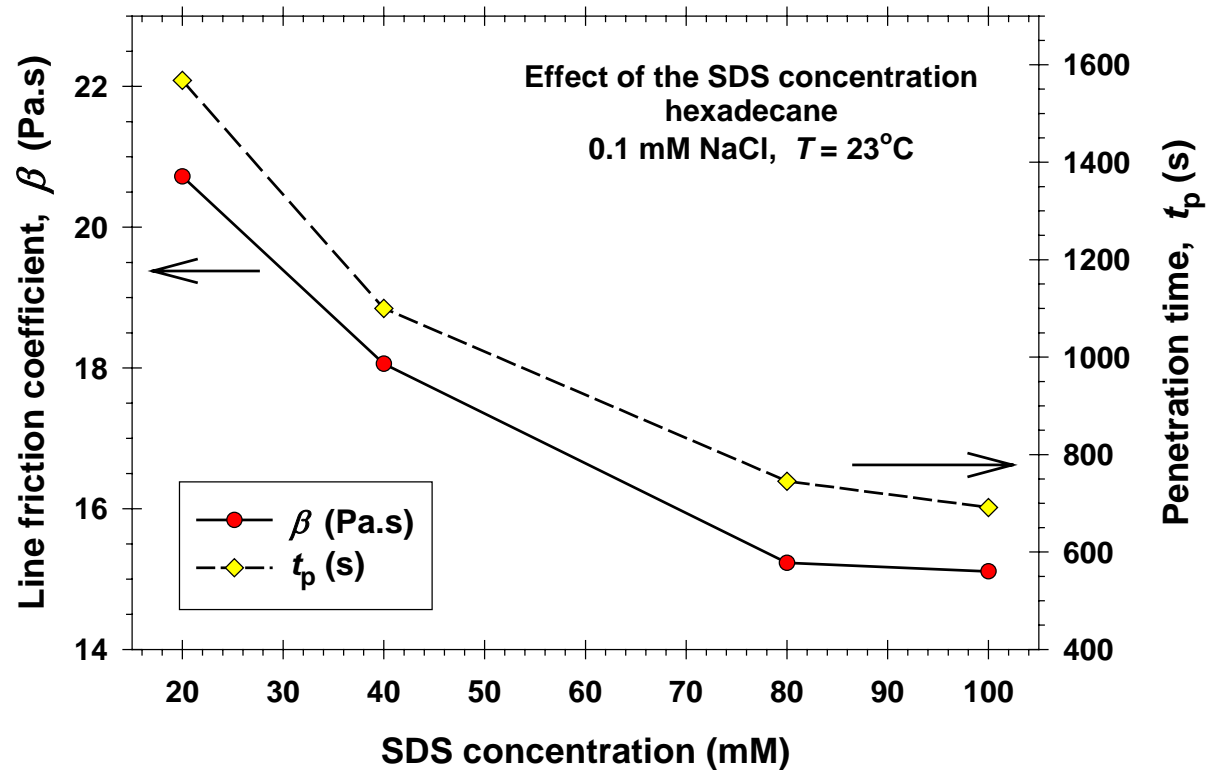
$$\Delta\sigma \equiv \sigma_{os}(c_{eq}/2) - \sigma_{ws}(c_{eq}/2)$$

$\alpha(t)$  is known from the experiment; **adjustable** parameters:  $\beta$ ,  $\Delta\sigma$ ,  $t_p$  and  $t_{in}$ .

Excellent agreement between theory and experiment is obtained!



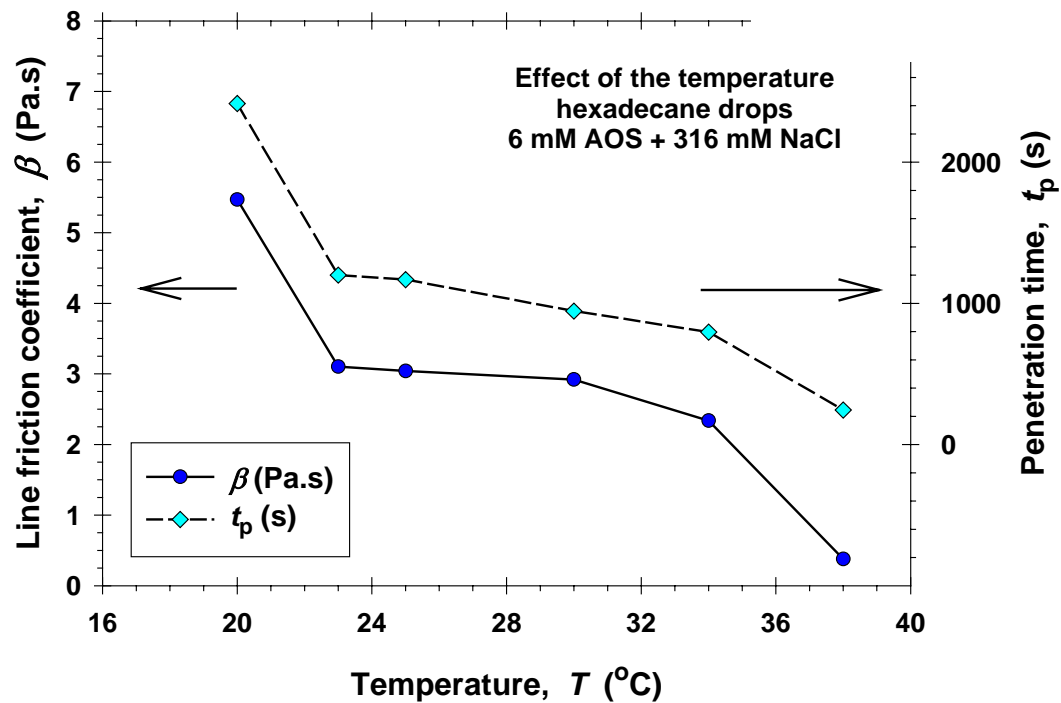
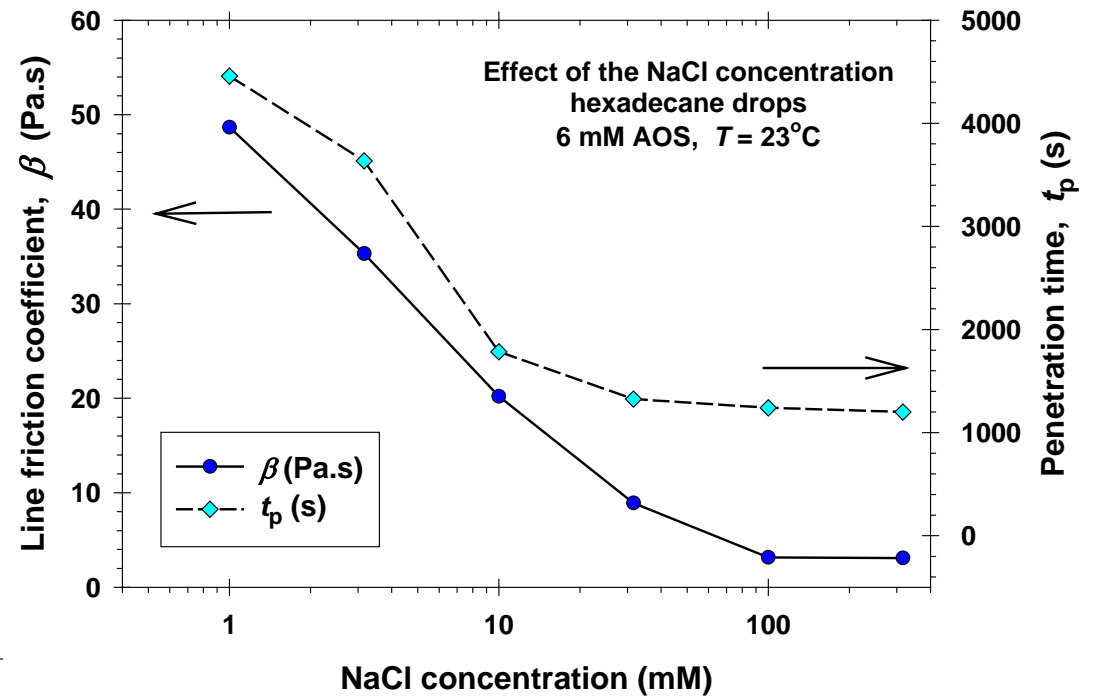
## Effect of Surfactant on Line Friction Coefficient and Penetration Time



The detected effect of **surfactant** on  $\beta$  and  $t_p$  is most probably related to its role for **hydrophilization** and/or **removal** of the **hydrophobic coverage (gloss)** of the glass surface.

## Effects of Salt and Temperature

The **salt** facilitates the surfactant adsorption.



The **temperature** is known to reduce the **viscous** effects and accelerate the **diffusion** processes.



## Conclusions

1. The increase of **temperature**, **surfactant** and **salt concentrations** accelerate the **oil-drop detachment**.
2. The spontaneous drop detachment is due to **penetration of water** in a **thin (gel) layer** at the surface of glass.
3. The data are excellently fitted by the **dynamic Young equation**, and the **line friction coefficient**,  $\beta$ , is determined.

